

## **A Computational Study of a Large Network with Arithmetic Progression on Pessimistic Time Estimate**

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**Abstract:** *The paper aspires to conclude whether Arithmetic Progression (A.P) in a particular case will substantiate a network or not. A huge network is considered in a specific way with 124 activities which are formed with 94 nodes. A.P is implemented on pessimistic time estimate (m) among the three time estimates namely optimistic, most likely and pessimistic. An algorithmic study has been performed on the network. Elite noteworthy results are launched. All float values are also ciphered. Critical path is delineated and project analysis has been followed up. Periodical analysis is attained with standard normal distribution curves.*

**Keywords:** *Network, Time estimates, Float, Critical path, Normal distribution.*

AMS Classification: 90-08, 90B10, 90C90

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### **1. INTRODUCTION**

Total float values play a vital role in networks. It is very useful to identify the critical path in an effective manner. There are only three possibilities for total float values i.e. positive, negative and zero. Total float value comes positive only when the resources are extra. In such case one has the liberty to reallocate the required resources. Total float values become negative in the case of the resources which are not adequate and also activity may not be finite. In such case extra resources are to be included. Total float values will be zero when resources are sufficient to complete the activity. The critical path can also be classified as 'the delay took place in its start time will cause a further delay in the culmination of entire project'.

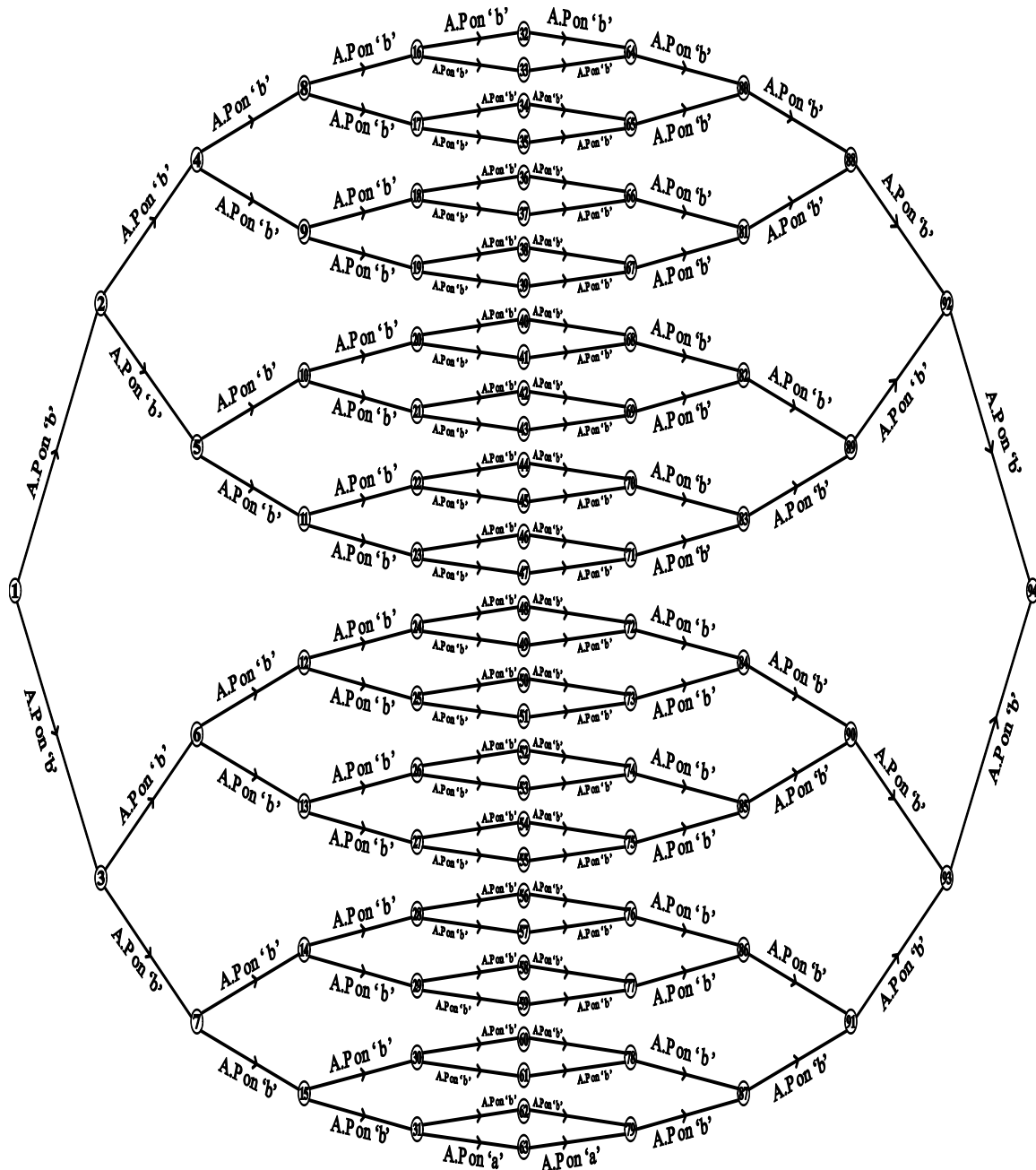
Acharyulu,K.V.L.N et.al. [1-5] discussed on Networks with various progressions. S.D Sharma [6] specified many useful applications of PERT&CPM in 1999. PERT algorithm was employed on various models by Billy E.Gillett [7] in 1979.Levin and Kirkpatrick [9] disclosed about planning and control with PERT and CPM in 1966.Wiest and Levy [8] explained the concept of PERT/CPM elaborately for beginners of operations research in 1969.

In the present work, it is aimed to clarify whether Arithmetic Progression (A.P) in a particular case will substantiate a network or not. A huge network is considered in a specific way with 124

activities which are formed with 94 nodes. A.P is applied on pessimistic time estimate (m) among the three time estimates. A scientific study has been employed on the network. Some noteworthy results are obtained. All float values are also determined. Critical path is illustrated and project analysis has been carried out. Periodical analysis is put through with standard normal distribution curves.

**2. BASIC CONSTRUCTION OF NETWORK**

A network is constituted with 94 nodes and 124 activities in a scientific way for analyzing the influence of Arithmetic Progression. A.P is used on pessimistic time estimate (m) in case (II) among the three estimates.



**Fig.1:** Network diagram with 124 activities and 94 nodes

### 3. PRELIMINARIES AND NOTATIONS

- **TE**= Earliest expected completion time of event (TE)
- **Def:** For the fixed value of  $j=TE(j)=\text{Max}[TE(i)+ET(i,j)]$  which ranges over all activities from  $i-j$ .
- **TL**= Latest allowable event completion time (TL)
- **Def:** For the fixed value of  $i=TL(i)=\text{Min}[TL(j)+ET(i,j)]$  which ranges over all activities from  $i-j$ .
- **ET**= Expected completion time of activity (I,J)
- **a**= Optimistic time estimate
- **m**= Most likely time estimate
- **b**= Pessimistic time estimate
- **ES** = Earliest start of an activity
- **EF** = Earliest finish of an activity
- **LS** = Latest start of an activity
- **LF** = Latest finish of an activity
- **TF** = Total Float
- **Def:** TF of activity  $i-j = LF_{i-j}-EF_{i-j}$  (or)  $LS_{i-j}-ES_{i-j}$
- **FF** = Free Float
- **Def:** FF of activity  $i-j = TF - (TL-TE)$  of node  $j$
- **IF** = Independent Float
- **Def:** IF of activity  $i-j = FF - (TL-TE)$  of node  $i$
- **SE**=Slack event time
- **CPI**=Critical Path Indicator
- **SCT**= Scheduled Time
- **$\sigma$**  = Standard deviation of project length

### 4. MATERIAL AND METHODS

Step 1: Draw the project network completion time

Step 2: Compute the expected duration of each activity by using the formula  $ET = \frac{a+4m+b}{6}$

From the time estimates a,m and p, calculate the expected variance.  $\sigma^2$  of each activity

Step 3: Calculate TE, TL

Step 4: Find Total Float, Free Float and Independent Float

Step 5: Find the critical path and identify the critical activities

Step 6: Compute project length which is a square root to sum of variance of all the critical activities.

Step 7: we can estimate the probability of completing project within specified time from the standard normal variable  $Z = \frac{SCT-ETC}{\sigma}$ , Where SCT is scheduled Completion time of event, ETC is expected completion time of the Project,  $\sigma$  =standard deviation of project length and also by using the standard normal curve.

### 5. RESULTS

With the help of CPM and PERT algorithm on the Network, the critical path is incurred from Table-1 which is illustrated with all activities, Time estimates, ET, Variance.ES, EF, LS, LF and all Float values. The Critical path indicator renders the critical activities in Table-1.

**Table-1**

Activity	Time Estimates			ET	$\sigma^2$	Earliest[E]		Latest[L]		TF	FF	IF	CPI
	a	m	b			ES	EF	LS	LF				
1-2	1	2	1.5	1.75	0.0069	0	1.75	124	125.75	124	0	0	
1-3	3	4	3.5	3.75	0.0069	0	3.75	0	3.75	0	0	0	*

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2-4	5	6	5.5	5.75	0.006 9	1.75	7.5	185.75	191.5	184	0	-124	
2-5	7	8	7.5	7.75	0.006 9	1.75	9.5	125.75	133.5	124	0	-124	
3-6	9	10	9.5	9.75	0.006 9	3.75	13.5	63.75	73.5	60	0	0	
3-7	11	12	11.5	11.75	0.006 9	3.75	15.5	3.75	15.5	0	0	0	*
4-8	13	14	13.5	13.75	0.006 9	7.5	21.25	219.5	233.25	212	0	-184	
4-9	15	16	15.5	15.75	0.006 9	7.5	23.25	191.5	207.25	184	0	-184	
5-10	17	18	17.5	17.75	0.006 9	9.5	27.25	161.5	179.25	152	0	-124	
5-11	19	20	19.5	19.75	0.006 9	9.5	29.25	133.5	153.25	124	0	-124	
6-12	21	22	21.5	21.75	0.006 9	13.5	35.25	101.5	123.25	88	0	-60	
6-13	23	24	23.5	23.75	0.006 9	13.5	37.25	73.5	97.25	60	0	-60	
7-14	25	26	25.5	25.75	0.006 9	15.5	41.25	43.5	69.25	28	0	0	
7-15	27	28	27.5	27.75	0.006 9	15.5	43.25	15.5	43.25	0	0	0	*
8-16	29	30	29.5	29.75	0.006 9	21.25	51	245.25	275	224	0	-212	
8-17	31	32	31.5	31.75	0.006 9	21.25	53	233.25	265	212	0	-212	
9-18	33	34	33.5	33.75	0.006 9	23.25	57	219.25	253	196	0	-184	
9-19	35	36	35.5	35.75	0.006 9	23.25	59	207.25	243	184	0	-184	
10-20	37	38	37.5	37.75	0.006 9	27.25	65	191.25	229	164	0	-152	
10-21	39	40	39.5	39.75	0.006 9	27.25	67	179.25	219	152	0	-152	
11-22	41	42	41.5	41.75	0.006 9	29.25	71	165.25	207	136	0	-124	
11-23	43	44	43.5	43.75	0.006 9	29.25	73	153.25	197	124	0	-124	
12-24	45	46	45.5	45.75	0.006 9	35.25	81	135.25	181	100	0	-88	
12-25	47	48	47.5	47.75	0.006 9	35.25	83	123.25	171	88	0	-88	
13-26	49	50	49.5	49.75	0.006 9	37.25	87	109.25	159	72	0	-60	

13-27	51	52	51.5	51.75	0.006 9	37.25	89	97.25	149	60	0	-60	
14-28	53	54	53.5	53.75	0.006 9	41.25	95	81.25	135	40	0	-28	
14-29	55	56	55.5	55.75	0.006 9	41.25	97	69.25	125	28	0	-28	
15-30	57	58	57.5	57.75	0.006 9	43.25	101	55.25	113	12	0	0	
15-31	59	60	59.5	59.75	0.006 9	43.25	103	43.25	103	0	0	0	*
16-32	61	62	61.5	61.75	0.006 9	51	112.7 5	279	340.75	228	0	-224	
16-33	63	64	63.5	63.75	0.006 9	51	114.7 5	275	338.75	224	0	-224	
14-34	65	66	65.5	65.75	0.006 9	53	118.7 5	269	334.75	216	0	-212	
17-35	67	68	67.5	67.75	0.006 9	53	120.7 5	265	332.75	212	0	-212	
18-36	69	70	69.5	69.75	0.006 9	57	126.7 5	257	326.75	200	0	-196	
18-37	71	72	71.5	71.75	0.006 9	57	128.7 5	253	324.75	196	0	-196	
19-38	73	74	73.5	73.75	0.006 9	59	132.7 5	247	320.75	188	0	-184	
19-39	75	76	75.5	75.75	0.006 9	59	134.7 5	243	318.75	184	0	-184	
20-40	77	78	77.5	77.75	0.006 9	65	142.7 5	233	310.75	168	0	-164	
20-41	79	80	79.5	79.75	0.006 9	65	144.7 5	229	308.75	164	0	-164	
21-42	81	82	81.5	81.75	0.006 9	67	148.7 5	223	304.75	156	0	-152	
21-43	83	84	83.5	83.75	0.006 9	67	150.7 5	219	302.75	152	0	-152	
22-44	85	86	85.5	85.75	0.006 9	71	156.7 5	211	296.75	140	0	-136	
22-45	87	88	87.5	87.75	0.006 9	71	158.7 5	207	294.75	136	0	-136	
23-46	89	90	89.5	89.75	0.006 9	73	162.7 5	201	290.75	128	0	-124	
23-47	91	92	91.5	91.75	0.006 9	73	164.7 5	197	288.75	124	0	-124	
24-48	93	94	93.5	93.75	0.006 9	81	174.7 5	185	278.75	104	0	-100	
24-49	95	96	95.5	95.75	0.006 9	81	176.7 5	181	276.75	100	0	-100	

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25-50	97	98	97.5	97.75	0.006 9	83	180.7 5	175	272.75	92	0	-88	
25-51	99	10 0	99.5	99.75	0.006 9	83	182.7 5	171	270.75	88	0	-88	
26-52	10 1	10 2	101. 5	101.7 5	0.006 9	87	188.7 5	163	264.75	76	0	-72	
26-53	10 3	10 4	103. 5	103.7 5	0.006 9	87	190.7 5	159	262.75	72	0	-72	
27-54	10 5	10 6	105. 5	105.7 5	0.006 9	89	194.7 5	153	258.75	64	0	-60	
27-55	10 7	10 8	107. 5	107.7 5	0.006 9	89	196.7 5	149	256.75	60	0	-60	
28-56	10 9	11 0	109. 5	109.7 5	0.006 9	95	204.7 5	139	248.75	44	0	-40	
28-57	11 1	11 2	111. 5	111.7 5	0.006 9	95	206.7 5	135	246.75	40	0	-40	
29-58	11 3	11 4	113. 5	113.7 5	0.006 9	97	210.7 5	129	242.75	32	0	-28	
29-59	11 5	11 6	115. 5	115.7 5	0.006 9	97	212.7 5	125	240.75	28	0	-28	
30-60	11 7	11 8	117. 5	117.7 5	0.006 9	101	218.7 5	117	234.75	16	0	-12	
30-61	11 9	12 0	119. 5	119.7 5	0.006 9	101	220.7 5	113	232.75	12	0	-12	
31-62	12 1	12 2	121. 5	121.7 5	0.006 9	103	224.7 5	107	228.75	4	0	0	
31-63	12 3	12 4	123. 5	123.7 5	0.006 9	103	226.7 5	103	226.75	0	0	0	*
32-64	12 5	12 6	125. 5	125.7 5	0.006 9	112.75	238.5	340.75	466.5	228	4	-224	
33-64	12 7	12 8	127. 5	127.7 5	0.006 9	114.75	242.5	338.75	466.5	224	0	-224	
34-65	12 9	13 0	129. 5	129.7 5	0.006 9	118.75	248.5	334.75	464.5	216	4	-212	
35-65	13 1	13 2	131. 5	131.7 5	0.006 9	120.75	252.5	332.75	464.5	212	0	-212	
36-66	13 3	13 4	133. 5	133.7 5	0.006 9	126.75	260.5	326.75	460.5	200	4	-196	
37-66	13 5	13 6	135. 5	135.7 5	0.006 9	128.75	264.5	324.75	460.5	196	0	-196	
38-67	13 7	13 8	137. 5	137.7 5	0.006 9	132.75	270.5	320.75	458.5	188	4	-184	
39-67	13 9	14 0	139. 5	139.7 5	0.006 9	134.75	274.5	318.75	458.5	184	0	-184	
40-68	14 1	14 2	141. 5	141.7 5	0.006 9	142.75	284.5	310.75	452.5	168	4	-164	

41-68	14 3	14 4	143. 5	143.7 5	0.006 9	144.75	288.5	308.75	452.5	164	0	-164	
42-69	14 5	14 6	145. 5	145.7 5	0.006 9	148.75	294.5	304.75	450.5	156	4	-152	
43-69	14 7	14 8	147. 5	147.7 5	0.006 9	150.75	298.5	302.75	450.5	152	0	-152	
44-70	14 9	15 0	149. 5	149.7 5	0.006 9	156.75	306.5	296.75	446.5	140	4	-136	
45-70	15 1	15 2	151. 5	151.7 5	0.006 9	158.75	310.5	294.75	446.5	136	0	-136	
46-71	15 3	15 4	153. 5	153.7 5	0.006 9	162.75	316.5	290.75	444.5	128	4	-124	
47-71	15 5	15 6	155. 5	155.7 5	0.006 9	164.75	320.5	288.75	444.5	124	0	-124	
48-72	15 7	15 8	157. 5	157.7 5	0.006 9	174.75	332.5	278.75	436.5	104	4	-100	
49-72	15 9	16 0	159. 5	159.7 5	0.006 9	176.75	336.5	276.75	436.5	100	0	-100	
50-73	16 1	16 2	161. 5	161.7 5	0.006 9	180.75	342.5	272.75	434.5	92	4	-88	
51-73	16 3	16 4	163. 5	163.7 5	0.006 9	182.75	346.5	270.75	434.5	88	0	-88	
52-74	16 5	16 6	165. 5	165.7 5	0.006 9	188.75	354.5	264.75	430.5	76	4	-72	
53-74	16 7	16 8	167. 5	167.7 5	0.006 9	190.75	358.5	262.75	430.5	72	0	-72	
54-75	16 9	17 0	169. 5	169.7 5	0.006 9	194.75	364.5	258.75	428.5	64	4	-60	
55-75	17 1	17 2	171. 5	171.7 5	0.006 9	196.75	368.5	256.75	428.5	60	0	-60	
56-76	17 3	17 4	173. 5	173.7 5	0.006 9	204.75	378.5	248.75	422.5	44	4	-40	
57-76	17 5	17 6	175. 5	175.7 5	0.006 9	206.75	382.5	246.75	422.5	40	0	-40	
58-77	17 7	17 8	177. 5	177.7 5	0.006 9	210.75	388.5	242.75	420.5	32	4	-28	
59-77	17 9	18 0	179. 5	179.7 5	0.006 9	212.75	392.5	240.75	420.5	28	0	-28	
60-78	18 1	18 2	181. 5	181.7 5	0.006 9	218.75	400.5	234.75	416.5	16	4	-12	
61-78	18 3	18 4	183. 5	183.7 5	0.006 9	220.75	404.5	232.75	416.5	12	0	-12	
62-79	18 5	18 6	185. 5	185.7 5	0.006 9	224.75	410.5	228.75	414.5	4	4	0	
63-79	18 7	18 8	187. 5	187.7 5	0.006 9	226.75	414.5	226.75	414.5	0	0	0	*

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64-80	18 9	19 0	189. 5	189.7 5	0.006 9	242.5	432.2 5	466.5	656.25	224	12	-212	
65-80	19 1	19 2	191. 5	191.7 5	0.006 9	252.5	444.2 5	464.5	656.25	212	0	-212	
66-81	19 3	19 4	193. 5	193.7 5	0.006 9	264.5	458.2 5	460.5	654.25	196	12	-184	
67-81	19 5	19 6	195. 5	195.7 5	0.006 9	274.5	470.2 5	458.5	654.25	184	0	-184	
68-82	19 7	19 8	197. 5	197.7 5	0.006 9	288.5	486.2 5	452.5	650.25	164	12	-152	
69-82	19 9	20 0	199. 5	199.7 5	0.006 9	298.5	498.2 5	450.5	650.25	152	0	-152	
70-83	20 1	20 2	201. 5	201.7 5	0.006 9	310.5	512.2 5	446.5	648.25	136	12	-124	
71-83	20 3	20 4	203. 5	203.7 5	0.006 9	320.5	524.2 5	444.5	648.25	124	0	-124	
72-84	20 5	20 6	205. 5	205.7 5	0.006 9	336.5	542.2 5	436.5	642.25	100	12	-88	
73-84	20 7	20 8	207. 5	207.7 5	0.006 9	346.5	554.2 5	434.5	642.25	88	0	-88	
74-85	20 9	21 0	209. 5	209.7 5	0.006 9	358.5	568.2 5	430.5	640.25	72	12	-60	
75-85	21 1	21 2	211. 5	211.7 5	0.006 9	368.5	580.2 5	428.5	640.25	60	0	-60	
76-86	21 3	21 4	213. 5	213.7 5	0.006 9	382.5	596.2 5	422.5	636.25	40	12	-28	
77-86	21 5	21 6	215. 5	215.7 5	0.006 9	392.5	608.2 5	420.5	636.25	28	0	-28	
78-87	21 7	21 8	217. 5	217.7 5	0.006 9	404.5	622.2 5	416.5	634.25	12	12	0	
79-87	21 9	22 0	219. 5	219.7 5	0.006 9	414.5	634.2 5	414.5	634.25	0	0	0	*
80-88	22 1	22 2	221. 5	221.7 5	0.006 9	444.25	666	656.25	878	212	28	-184	
81-88	22 3	22 4	223. 5	223.7 5	0.006 9	470.25	694	654.25	878	184	0	-184	
82-89	22 5	22 6	225. 5	225.7 5	0.006 9	498.25	724	650.25	876	152	28	-124	
83-89	22 7	22 8	227. 5	227.7 5	0.006 9	524.25	752	648.25	876	124	0	-124	
84-90	22 9	23 0	229. 5	229.7 5	0.006 9	554.25	784	642.25	872	88	28	-60	
85-90	23 1	23 2	231. 5	231.7 5	0.006 9	580.25	812	640.25	872	60	0	-60	
86-91	23 3	23 4	233. 5	233.7 5	0.006 9	608.25	842	636.25	870	28	28	0	



87-91	23 5	23 6	235. 5	235.7 5	0.006 9	634.25	870	634.25	870	0	0	0	*
88-92	23 7	23 8	237. 5	237.7 5	0.006 9	694	931.7 5	878	1115.7 5	184	60	-124	
89-92	23 9	24 0	239. 5	239.7 5	0.006 9	752	991.7 5	876	1115.7 5	124	0	-124	
90-93	24 1	24 2	241. 5	241.7 5	0.006 9	812	1053. 8	872	1113.7 5	60	60	0	
91-93	24 3	24 4	243. 5	243.7 5	0.006 9	870	1113. 8	870	1113.7 5	0	0	0	*
92-94	24 5	24 6	245. 5	245.7 5	0.006 9	991.75	1237. 5	1115.7 5	1361.5	124	12 4	0	
93-94	24 7	24 8	247. 5	247.7 5	0.006 9	1113.7 5	1361. 5	1113.7 5	1361.5	0	0	0	*

Critical path is obtained as below

$$1 \xrightarrow{3.75} 3 \xrightarrow{11.75} 7 \xrightarrow{27.75} 15 \xrightarrow{59.75} 31 \xrightarrow{123.75} 63 \xrightarrow{187.75} 79 \xrightarrow{219.75} 87 \xrightarrow{235.75} 91 \xrightarrow{243.75} 93 \xrightarrow{247.75} 94$$

Project Length is defined as  $\sqrt{\text{Sum of Variances of each Critical activity}}$

$$\text{i.e Project Length} = \sqrt{0.0069 + 0.0069 + 0.0069 + 0.0069 + 0.0069 + 0.0069 + 0.0069 + 0.0069 + 0.0069 + 0.0069} = 0.2626$$

The values of TE, TL and SE corresponding to every node are tabulated in table (2).

Table-2

Nodes	TE	TL	SE	Nodes	TE	TL	SE
1	0	0	0	48	174.75	278.75	104
2	1.75	125.75	124	49	176.75	276.75	100
3	3.75	3.75	0	50	180.75	272.75	92
4	7.5	191.5	184	51	182.75	270.75	88
5	9.5	133.5	124	52	188.75	264.75	76
6	13.5	73.5	60	53	190.75	262.75	72
7	15.5	15.5	0	54	194.75	258.75	64
8	21.25	233.25	212	55	196.75	256.75	60
9	23.25	207.25	184	56	204.75	248.75	44
10	27.25	179.25	152	57	206.75	246.75	40
11	29.25	153.25	124	58	210.75	242.75	32
12	35.25	123.25	88	59	212.75	240.75	28
13	37.25	97.25	60	60	218.75	234.75	16
14	41.25	69.25	28	61	220.75	232.75	12

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15	43.25	43.25	0	62	224.75	228.75	4
16	51	275	224	63	226.75	226.75	0
17	53	265	212	64	242.5	466.5	224
18	57	253	196	65	252.5	464.5	212
19	59	243	184	66	264.5	460.5	196
20	65	229	164	67	274.5	458.5	184
21	67	219	152	68	288.5	452.5	164
22	71	207	136	69	298.5	450.5	152
23	73	197	124	70	310.5	446.5	136
24	81	181	100	71	320.5	444.5	124
25	83	171	88	72	336.5	436.5	100
26	87	159	72	73	346.5	434.5	88
27	89	149	60	74	358.5	430.5	72
28	95	135	40	75	368.5	428.5	60
29	97	125	28	76	382.5	422.5	40
30	101	113	12	77	392.5	420.5	28
31	103	103	0	78	404.5	416.5	12
32	112.75	340.75	228	79	414.5	414.5	0
33	114.75	338.75	224	80	444.25	656.25	212
34	118.75	334.75	216	81	470.25	654.25	184
35	120.75	332.75	212	82	498.25	650.25	152
36	126.75	326.75	200	83	524.25	648.25	124
37	128.75	324.75	196	84	554.25	642.25	88
38	132.75	320.75	188	85	580.25	640.25	60
39	134.75	318.75	184	86	608.25	636.25	28
40	142.75	310.75	168	87	634.25	634.25	0
41	144.75	308.75	164	88	694	878	184
42	148.75	304.75	156	89	752	876	124
43	150.75	302.75	152	90	812	872	60
44	156.75	296.75	140	91	870	870	0
45	158.75	294.75	136	92	991.75	1115.75	124
46	162.75	290.75	128	93	1113.75	1113.75	0

47	164.75	288.75	124	94	1361.5	1361.5	0
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### 6. PERIODICAL ANALYSIS

Periodical analysis is carried out with some particular schedule times. The standard normal variables with the probability from zero to one are made out. The percentage of probabilities of completion of the Project are computed and given in the following Table-3.

Table-3

ST	TE	Z	probability	Probability (%)
1360	1361.5	-5.7121	0	0
1361	1361.5	-1.9040	0.0287	2.87
1362	1361.5	1.9040	0.9713	97.13
1363	1361.5	5.7121	1	1

The Standard Normal Curves are depicted from Fig.2-Fig.4

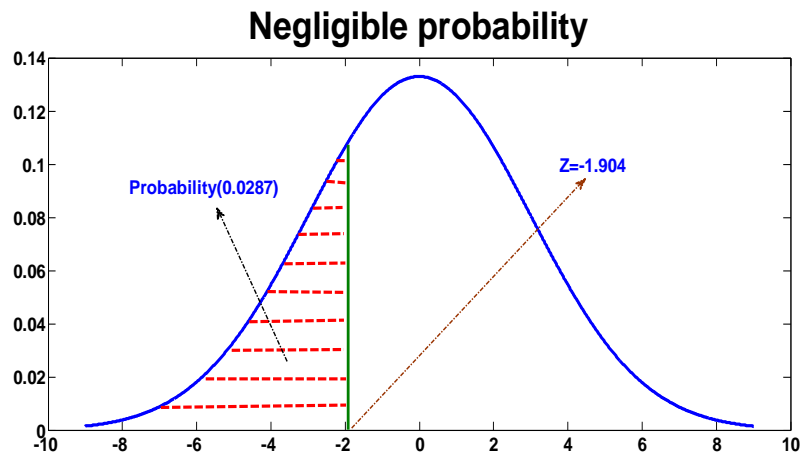


Fig.2

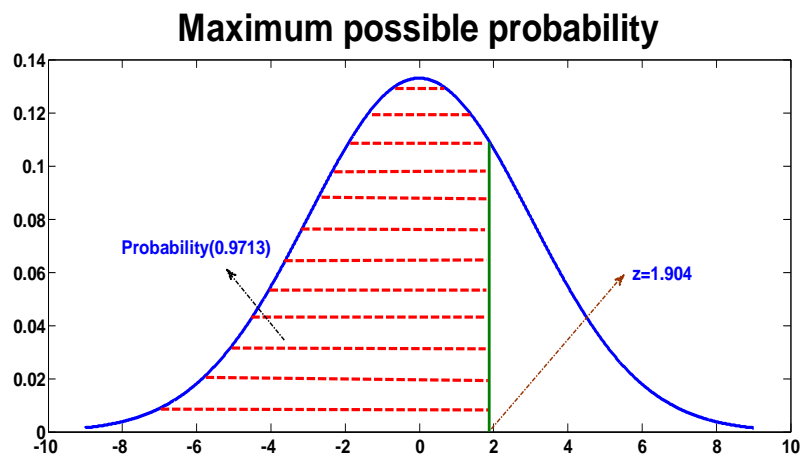
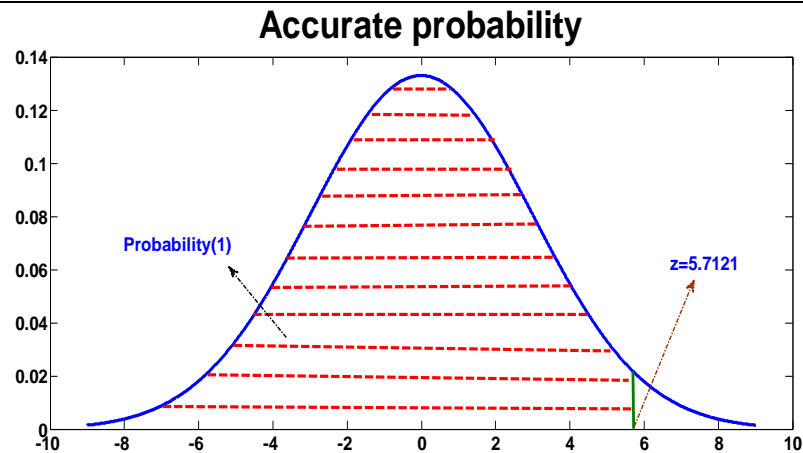


Fig.3



**Fig.4**

## 7. CONCLUSIONS

From the computational study, the following conclusions are obtained.

- (i).The influence of A.P on network with SCT and ETC is accomplished as below
  - (a).A.P endorses incisively only when SCT is greater than ETC.
  - (b).A.P does not endorse when SCT is less than or equal to ETC.
  - (c). Standard Normal Distribution curves supply the percentage of possibilities of the Project.
- (ii).Constant Variances can be traced in any activity of the Network.
- (iii).In Critical Path
  - (a).All Total Float values of Critical activities are vanished.
  - (b).The value of Slack event of each node in critical path is zero.
  - (c). TE and TL are equal at each node in critical path.
- (iv).In the data of Net work, A.P is looked at optimistic time estimate, the expected completion time of successive activity is magnified step by step.
- (v). A.P endorses the Network with the condition even though the network has huge size.

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